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A Study on Hydraulic Fracture Geometry using Macro-Scale Physical Simulation in Marine Shale Haifeng Fu

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A Study on Hydraulic Fracture Geometry using Macro-Scale Physical Simulation in Marine Shale

OUTLINE







Opportunities in Shale Gas Industry

- seismic technology
- horizontal well drilling
- multi-stage hydraulic fracturing





*EIA AEO 2011

- Challenge in China Shale Gas Stimulation
 - More complex geological conditions
 - Fracturing mechanism unclear.
 - □ Fracturing design method immature.



The Purpose of Physical Simulation

□ The effect of geological & pumping

conditions on SRV

□ Trying to solve three key questions









- Physical simulation is an effective way
- Observe HF geometry
 □ Single/Multiple/ fracture
- Test new fracturing process
 Massive fracturing
 Hybrid fracturing
- Modify acoustic location
 - □ Tensile/shear events



sandstone



Linestone



Fibre fracturing



Acoustic monitoring 5

• Large-scale test for hydraulic fracturing is useful.

Research Institute	Sample Dimension	Injection Pressure	Post-evaluation Method
China University of Petroleumn	300mm	20MPa	Manual Splitting
Delft University of Technology	350mm	35MPa	Active Accoustic Monitoring
University of California,Berkely	450mm	60MPa	Manual Splitting
TerraTek Company	914mm	69MPa	Manual Splitting
CNPC	914mm	69MPa	Passive Acoustic Monitoring Real-time





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OUTLINE

Technology of Natural Block Preparation.

Diamond Line-saw Cutting

• Sample standard dimension:

762(length) × 762(width) × 914mm(height)

- Larger block should be cut
- Shale is easy to crush due to brittleness



- Smaller block should be cemented
- Difference of mechanical property
- Numerical simulation of stress distribution









Technology of Hydraulic Fracturing Experiment.

Large Block Test System for Hydraulic Fracturing

Structure Diagram



Technical Parameters

- Maximum Loading pressure: 10000psi
- Maximum stress difference: 2000psi
- Maximum borehole diameter: 4.9in
- Maximum injection pressure 12000psi
- Maximum injection rate: 12L/min
- Acoustic monitoring : 24 channels

Large Block Test System for Hydraulic Fracturing

Areas of Investigation

- Fracture Initiation
- Fracture Containment
- Fracture Complexity
- Acoustic monitoring
- Perforation
- Shale Completion



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Acoustic monitoring

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Technology of Passive Acoustic Monitoring.

To describe fracture propagation in real-time

- Sensors at different sites.
- Signals emitted by fracturing are
 - located.
- Signals at the same time can
 - reflect fracture geometry.



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OUTLINE



1. Basic data

I type shale



- Higher clay content;
- Weathering;
- Easy to be crushed;



II type shale

- Lower clay content;
- > Tight ;
- Cut without damage;

Total rock x-ray diffraction analysis and Clay mineral

	Clay mineral relative content (%)						Total rock quantitative (%)					
Rock type	к	С	Ι	I/S	%S		Quart Z	Potassiu m feldspar	Plagio clase	Calci te	Dolomi te	Chromi te
Ι	5	20	36	39	10	44	28	1	7	9	9	2
Π		8	85	7	5	12	52		1	20	14	1
Tips	K: ka	olinite,	C:chl	orite, I:	illite, S	:sme	ctite, I/S: il	lite/smectit	te interla	yer, %S	: interlay	er ratio

2. Results.

Summary of test conditions and results

Test number	Rock type	⊡σ _{v,H,h} (MPa)	K _h	Viscosity (cP)	Pump rate(cm ³ /s)	P _{net} ,D	Fracture geometry
1	Ι	24,24,1 0	1. 4	5	8.33	0.21	Complex, many nature fractures dilated
2	Ι	13,13,1 0	0. 3	5	166.67	0	Simple, one fracture connected one discontinuity
3	Π	13,13,1 0	0. 3	5	67	3.02	Complex, three nature fractures dilated
4	Π	13,13,1 0	0.	all	the cor	nditi	ons lex, one fracture connected re fractures
5	Π	24,24,1 0	4	are t	ne sam in fie	e as Id	e fracture connected
6	Π	24,24,1 0	1. 4	150	8.33	0.39	Simple, only one hydraulic fracture

Note: Horizontal stress difference

 $K_h = (\sigma_H - \sigma_h) / \sigma_h$

Dimensionless net pressure

$$p_{net,D} = \frac{p_{net}}{\sigma_H - \sigma_h}$$







The existing and pattern of natural fractures determine hydraulic fracture geometry.

- More natural fractures, More complicated
- Higher injection pressure, More tortuosity



Test number	Rock type	⊡σ _{v,H,h} (MPa)	K _h	Viscosity (cP)	Pump rate(cm ³ /s)	P _{net^yD}
1	Ι	24,24,10	1.4	5	8.33	0.21
5	Π	24,24,10	1.4	5	8.33	0.12

Case 2

Lower horizontal stress difference and fluid viscosity, More complex geometry, as test 3 and test 6 showed.



Test number	⊡σ _{v,H,h} (MPa)	Viscosity (cP)	Pump rate(cm ³ /s)	P _{net} ,D
3	13,13,10	5	166.67	3.02
6	24,24,10	150	8.33	0.39

Case 2

- Test4 and test5 show less complex fracture geometry can exist in some cases.
- It is difficult to produce complex fracture geometry with higher viscous fluid.



Test number	⊡σV,H,h (MPa)	Viscosity (cP)	Pump rate(cm3/s)	Pnet,D
4	13,13,10	150	1	3.6
5	24,24,10	5	8.33	0.12

Case 2



$$p_{net,D} = \frac{p_{net}}{\sigma_H - \sigma_h}$$

Case 3

Application of Acoustic Monitoring in Lab



- Attenuation and anisotropy lead to locate acoustic event badly.
- Advanced locating needs to be improved in future.

Case 3

Rock failure mechanism analysis



- the tensile rupture is dominated in tight sandstone.
- the proportion of shear events is the largest in coal.
- Shear event or slippage is also usual in shale.

Conclusion

- **Large-scale physical simulation is an effective way to research.**
- More complex fracture with natural fractures、high net pressure 、low

stress difference and fluid viscosity.

Acoustic events corresponding to complex fracture will be investigated.





Thanks for your attention!



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